

FC Workshop 2015

Fuel cell systems for aircraft applications

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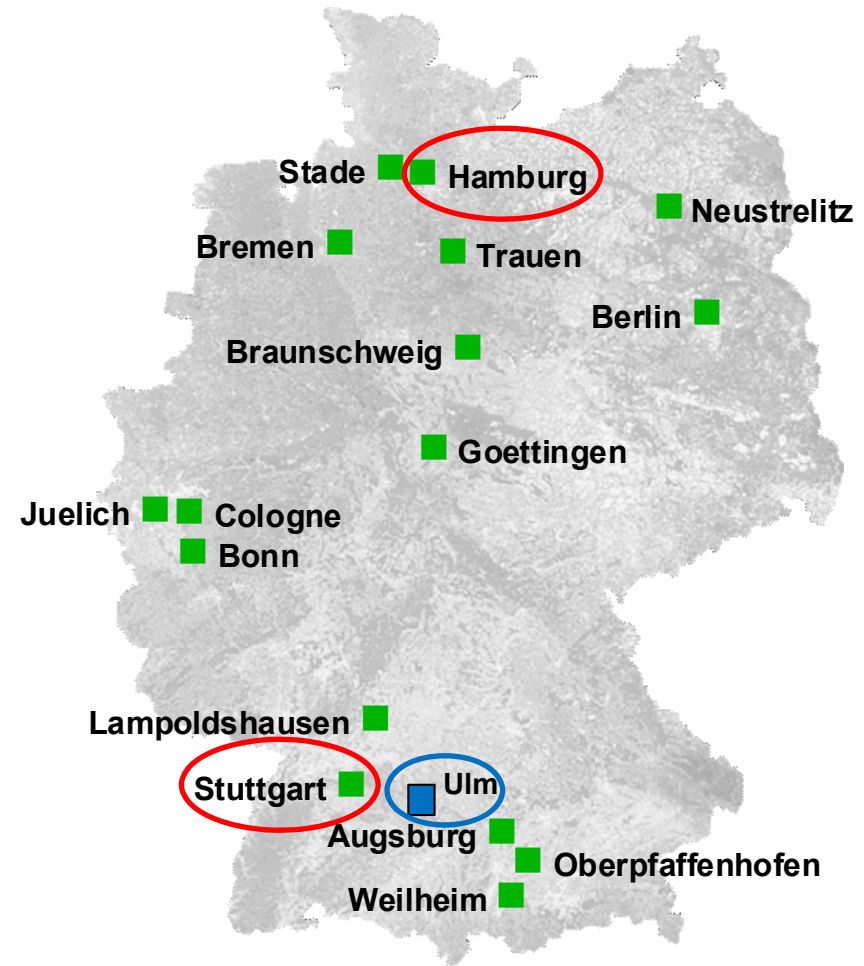
German Aerospace Center - Institute of Engineering Thermodynamics
University of Ulm - Institute of Energy Conversion and Energy Storage

Lampoldshausen, 15.09.2015



Aerospace Research Center and Space Agency of the Federal Republic of Germany (DLR)

- 7.700 employees
 - 16 national facilities
 - > 30 institutes and test facilities
 - offices in Brüssel, Paris, Washington
 - Test facilities in Almeria/Spain
-
- **ESI Energy System Integration, DLR**
 - Battery Systems and degradation
 - Fuel Cell Systems and degradation
 - Aircraft Applications MEA and AEA



University of Ulm – Institute of Energy Conversion and Energy Storage

Department of Hybrid Concepts

- Power Electronic Hardware, Controls and FC/Battery Power Management Systems

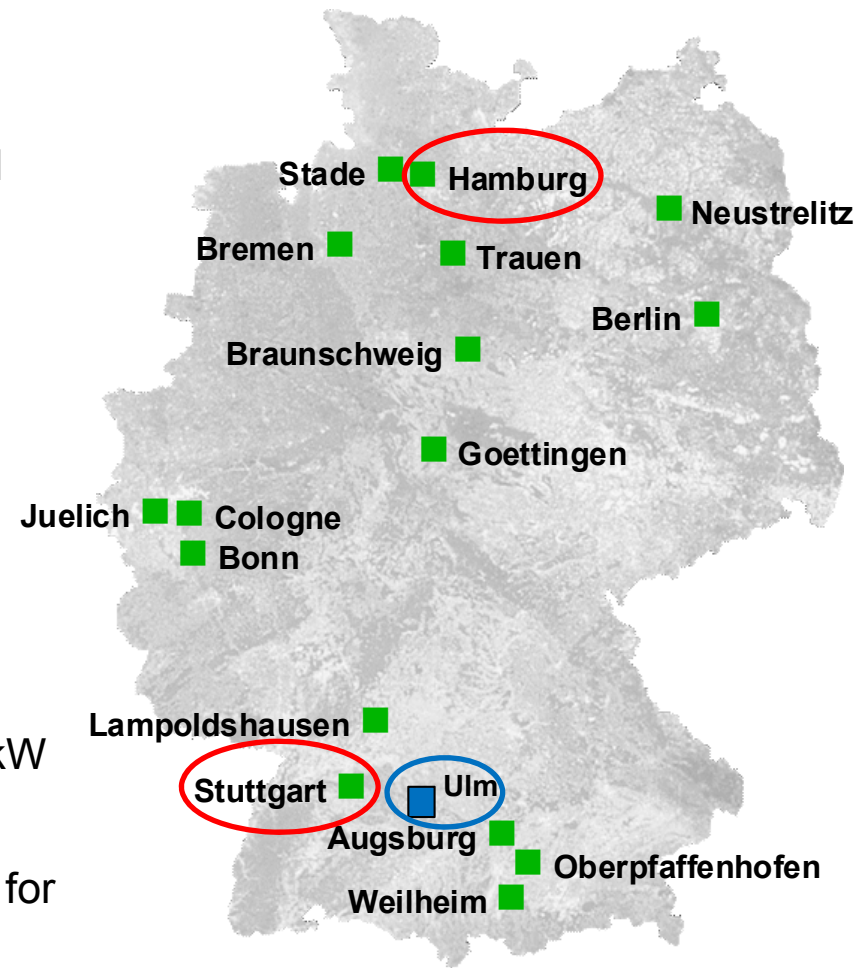
Department of Propulsion Research

- High power E-Machines, Generators

Applications: Aircraft applications,

Hardware/Teststand:

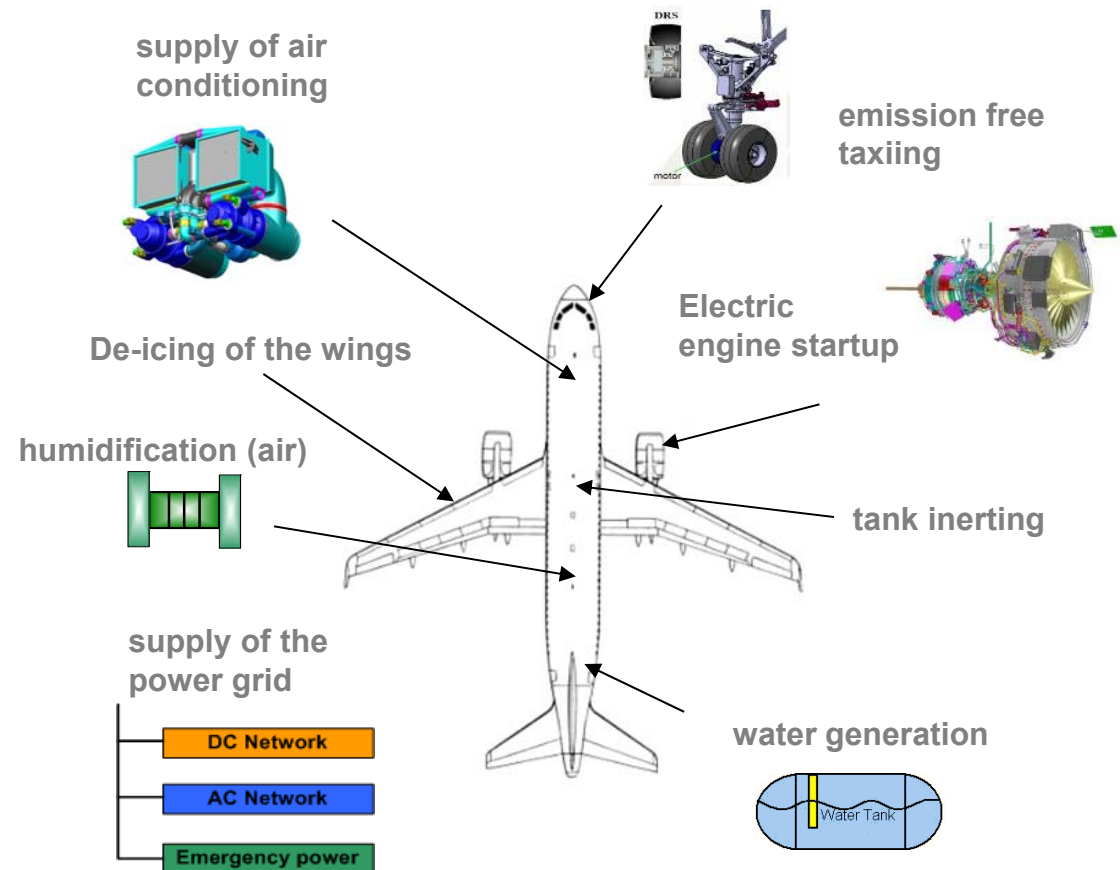
- ICE-Battery-E-Machine Hybrid up to 250kW
- Hydrogen infrastructure
- Low Pressure and Temperature chamber for components and complete systems



Potentials of fuel cells in aviation applications

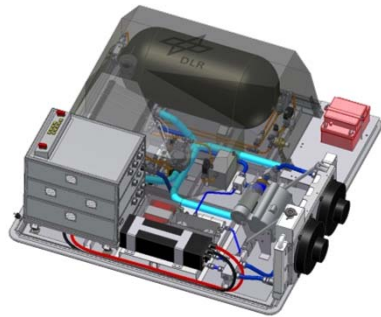
→ Multifunctional use of fuel cell systems in an aircraft

- electric energy supply
- emission free ground operation
→ Autonomous Taxiing
- electric Main Engine Start
- supply of air conditioning
- water production
(potable water and lavatory)
- waste heat recovery
(de-icing, warm water generation)
- prevention and suppression of fire and explosions
(tank inerting, cargo inerting)
- humidification of Cockpit air and/or cabin air



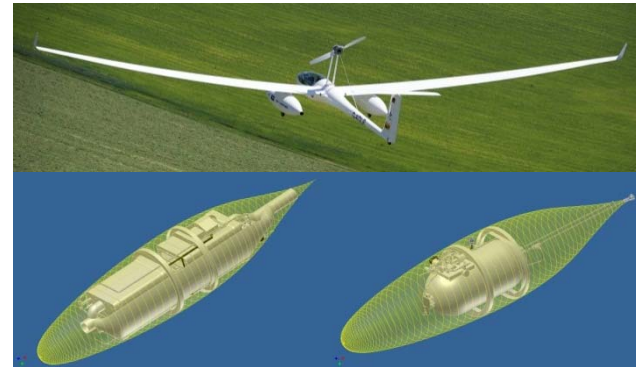
Fuel Cell Aircraft and Airport Applications at DLR Institute of Engineering Thermodynamics

Fuel Cell Technology Development Platform



Electric Energy, ODA, Water Source
(→ MFFC)
Energy Source for Emission Free Taxi

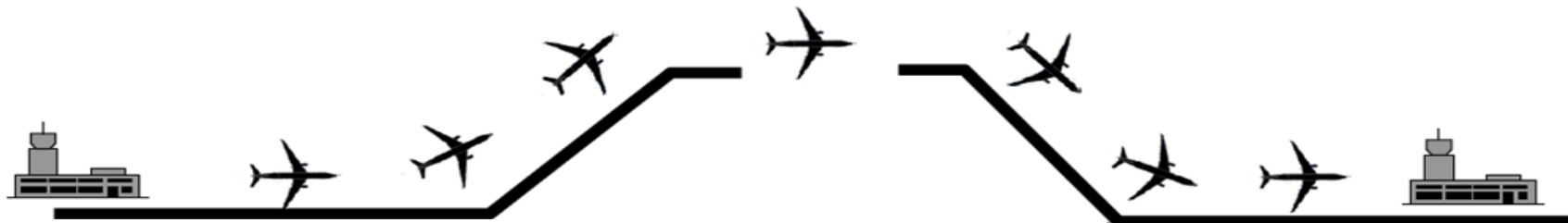
Modular Hybrid Development Platform EASA CS.22 and CS.23.Light



Flying Testrig for Fuel Cells and
Hybrids,
Emission Free Propulsion
for UAV and General Aviation
(4-6 Pax or 200 kg Payload)



Aircraft flight profile



$$0,25bar < P_{in_air} < 1bar$$



Impact of feed gas humidification to the water management of a PEMFC under aviation relevant conditions

Assumptions:

- Pressure difference between cathode inlet and outlet is neglected
- Water drag between cathode and anode is neglected
- O₂ – Concentration of cathode inlet gas is assumed to be 21 Vol.-%
- T_{in} = T_{Exhaust} – 10K

$$\lambda_{Cathode} = \frac{0,21 \cdot rH_{Exhaust} \cdot p_{Sat_H_2O_Exhaust}(T_{Exhaust}) - p_{Exhaust}}{\Psi \cdot p_{Exhaust} - rH_{Exhaust} \cdot (1 + \Psi) \cdot p_{Sat_H_2O_Exhaust}(T_{Exhaust})} \quad \text{with} \quad \Psi = \frac{p_{H_2O_In}}{p_{In} - p_{H_2O_In}} = \frac{rH_{In} \cdot p_{Sat_H_2O_In}(T_{In})}{p_{In} - rH_{In} \cdot p_{Sat_H_2O_In}(T_{In})}$$

$rH_{Exhaust}$ = Relative humidity of cathode exhaust gas

rH_{In} = Relative humidity of cathode inlet gas

p_{In} = Pressure of cathode inlet gas

$p_{Exhaust}$ = Pressure of cathode exhaust gas

$p_{H_2O_In}$ = Water vapor pressure of cathode inlet gas

$p_{Sat_H_2O_In}$ = Saturation vapor pressure of cathode inlet gas

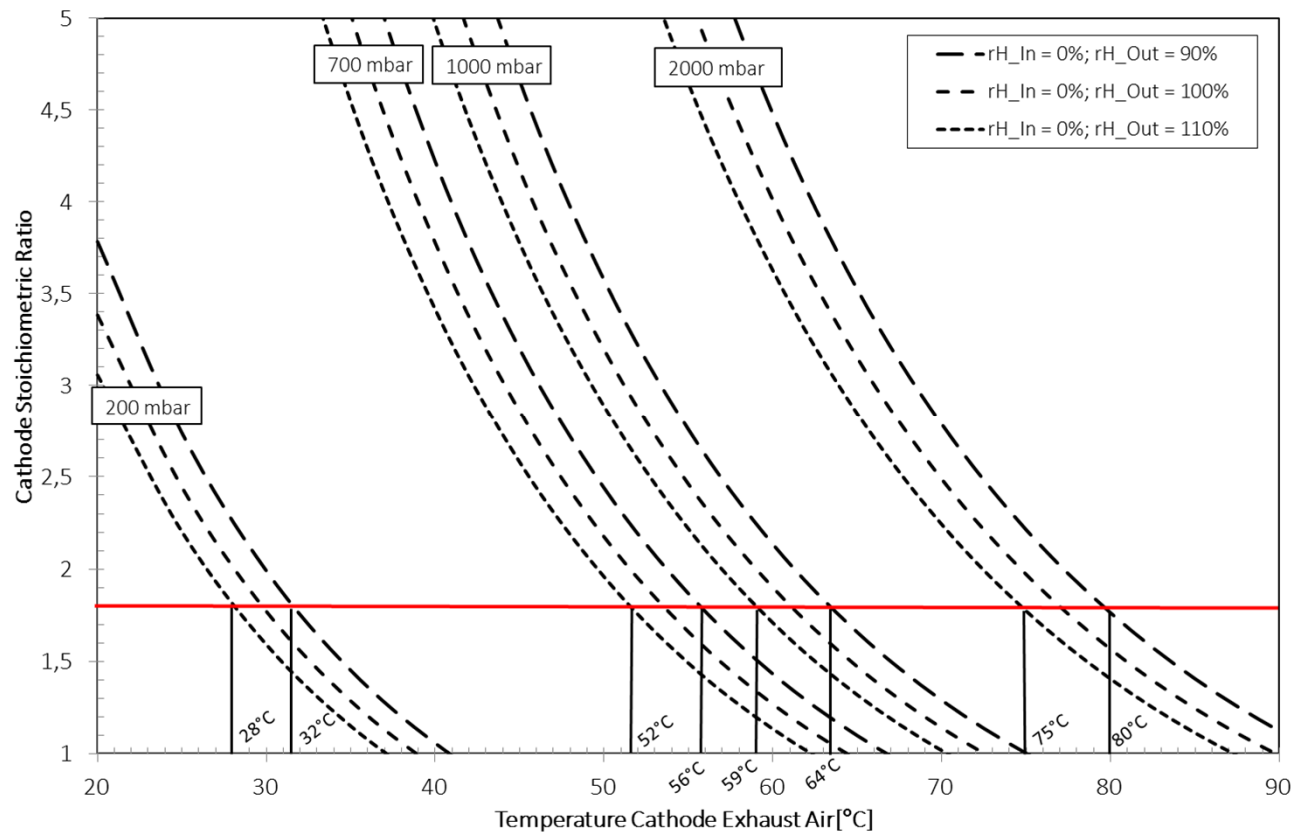
$p_{Sat_H_2O_Exhaust}$ = Saturation vapor pressure of cathode exhaust gas

T_{In} = Temperature of cathode inlet gas

$T_{Exhaust}$ = Temperature of cathode exhaust gas



Impact of aviation relevant operating parameters to the water management of a self-humidified PEMFC



System temperature control crucial for humidification

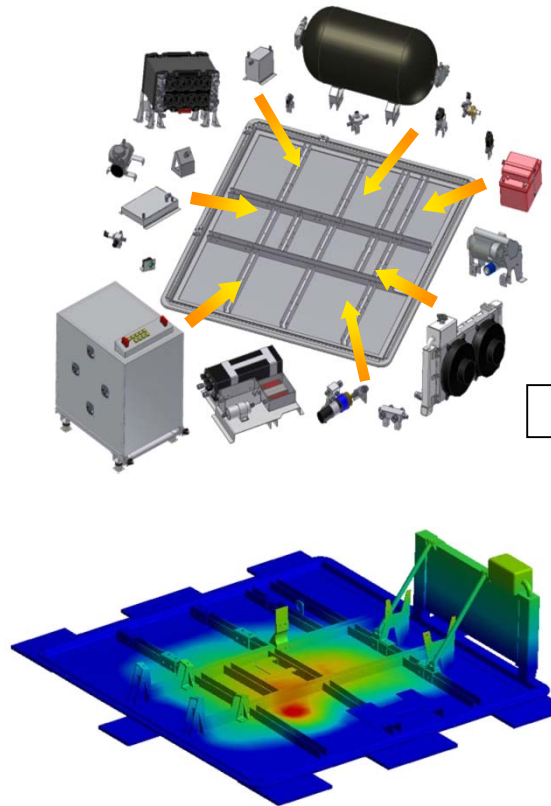
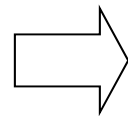
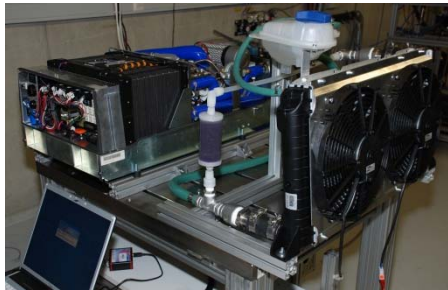


System build up:

Fuel Cell Technology Transfer to Aircraft Application

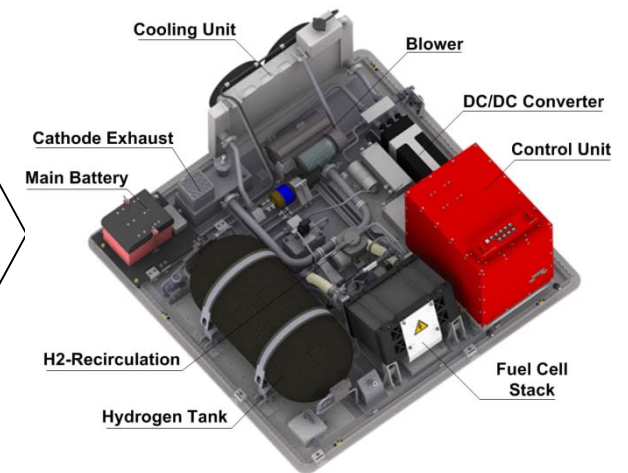
Aircraft Application (DO16xX)
Functionality, Architecture, BOP

FC System from Transport
Application



Mechanical Strength Simulation
Vibration, EMC, H2 Safety, Controls

**Airworthy technology
development platform**

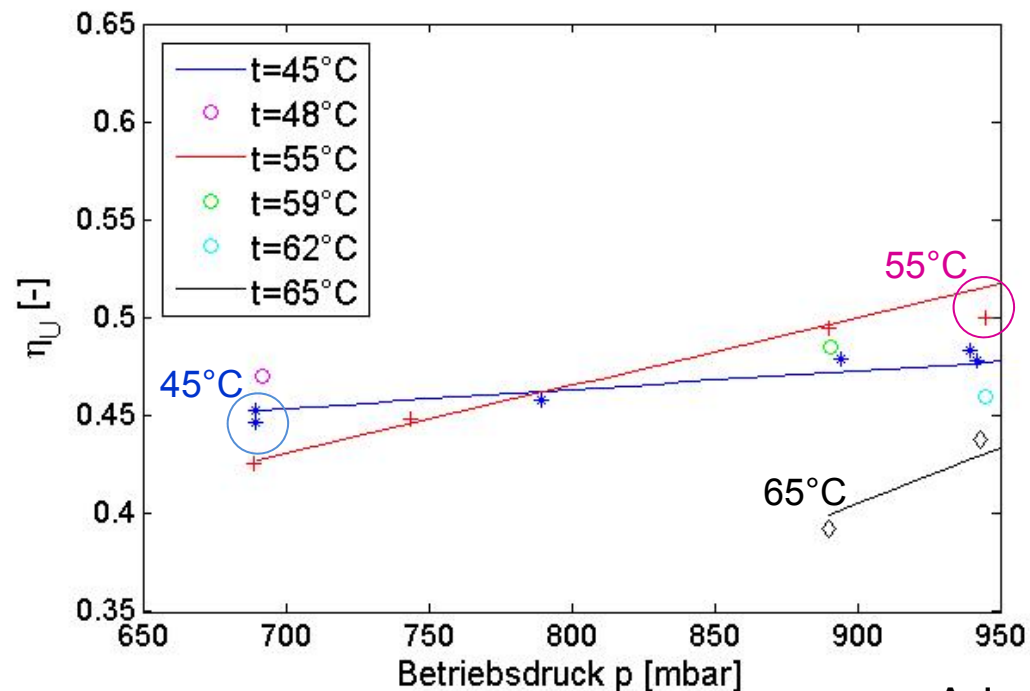


- Fuel cell
- DC/DC
- hydrogen storage



Fuel cell system efficiency as a function of cathode inlet pressure and relative humidity at the cathode outlet

System efficiency



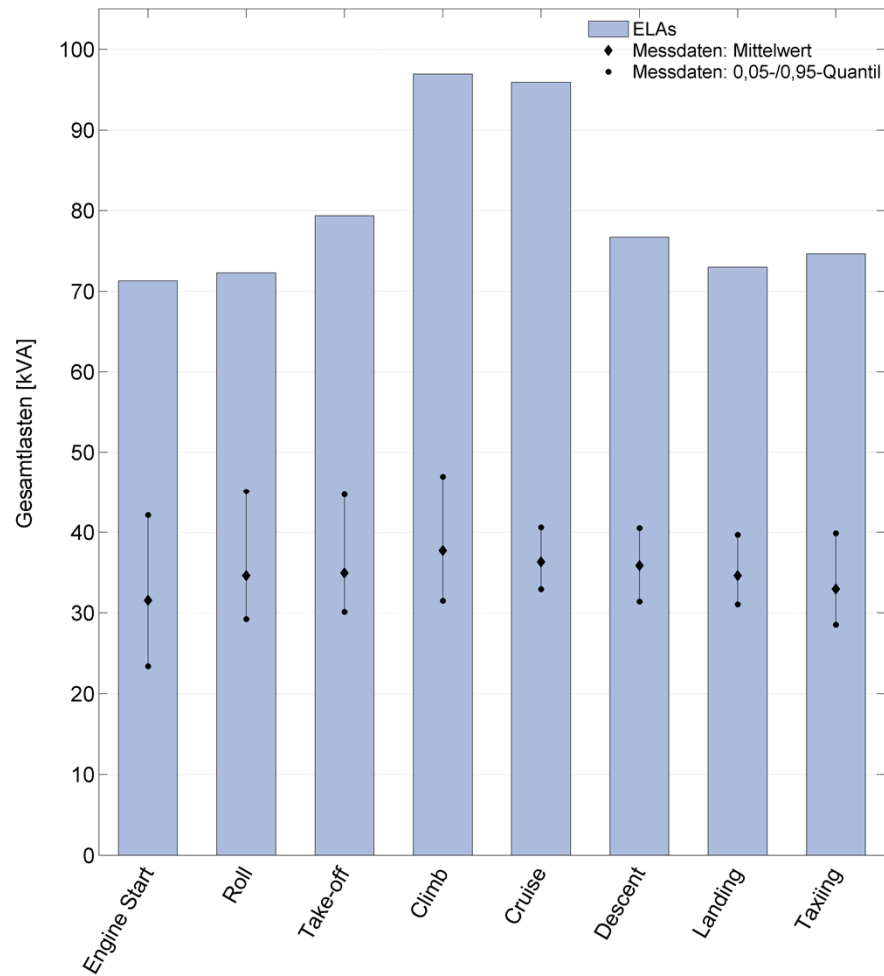
Temperature (cath out)	rHout (%) 950 mbar	rHout (%) 700 mbar
45	161	108
48	139	93
55	98	65
65	62	41

Adequate system temperature for optimal system efficiency ($I_{\text{Stack}} = 0,5 I_{\text{max}}$)



Fuel Cell System Topology

Electrical power assessment A320 (681 flights, 5 different A320)

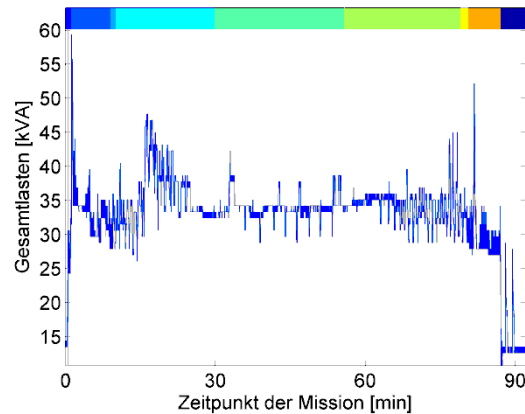


Average real world consumption lower than 50% of ELA

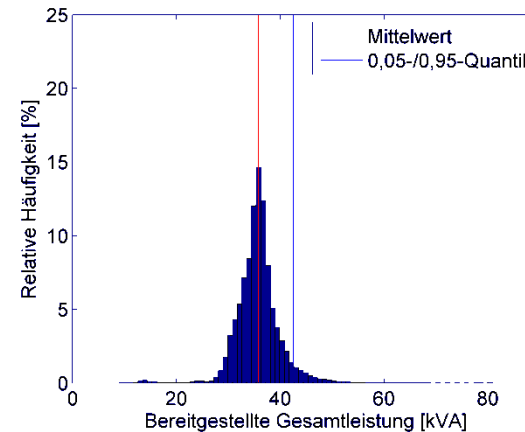


Electrical power data catalogue A320

Profiles electrical power

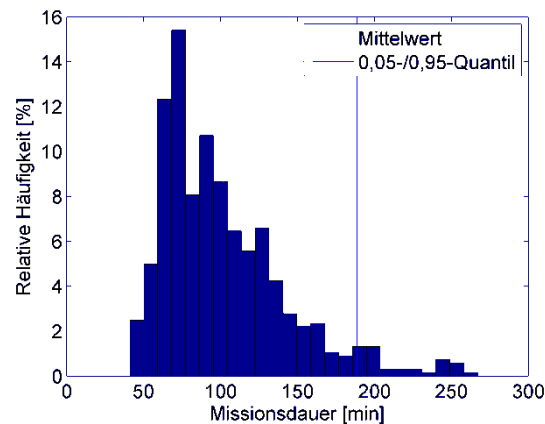


Overall Electrical power catalogue



- 681 Flights
- Flightphase definition based on ELA

Mission duration catalogue



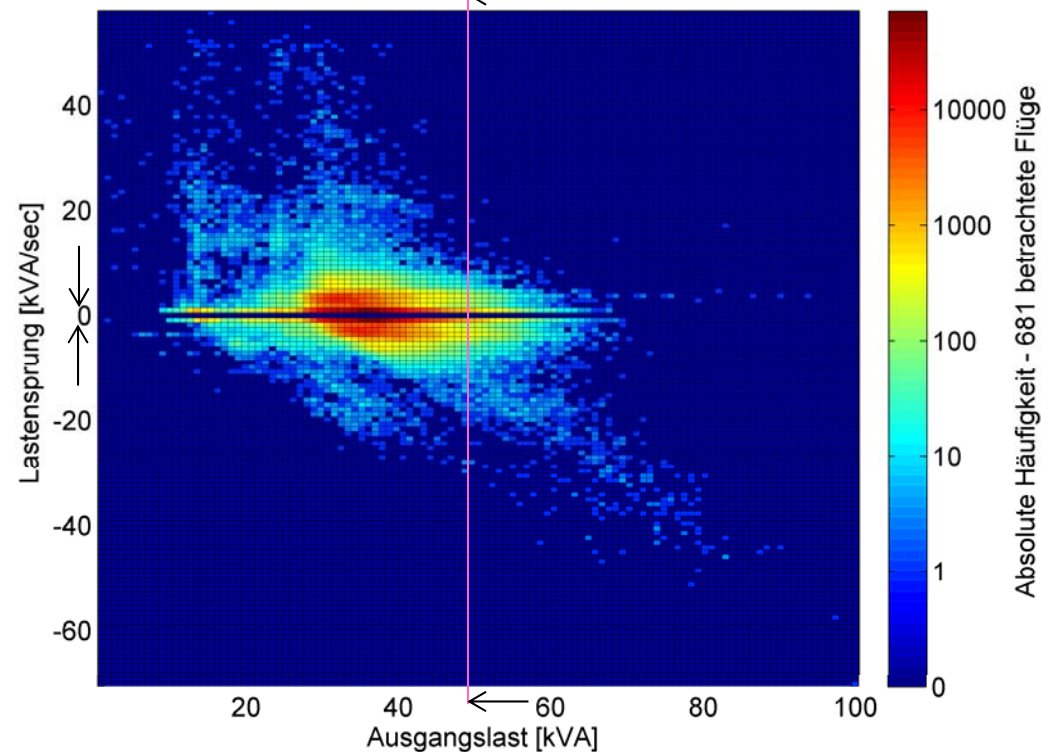
Average mission duration: ca. 100min
Average electrical power: ca. 36kW

→ Average 3,6kg H₂ /mission
(at 50% system efficiency)



Specific electric power distribution and dynamics A320

Electric power and electric power dynamics

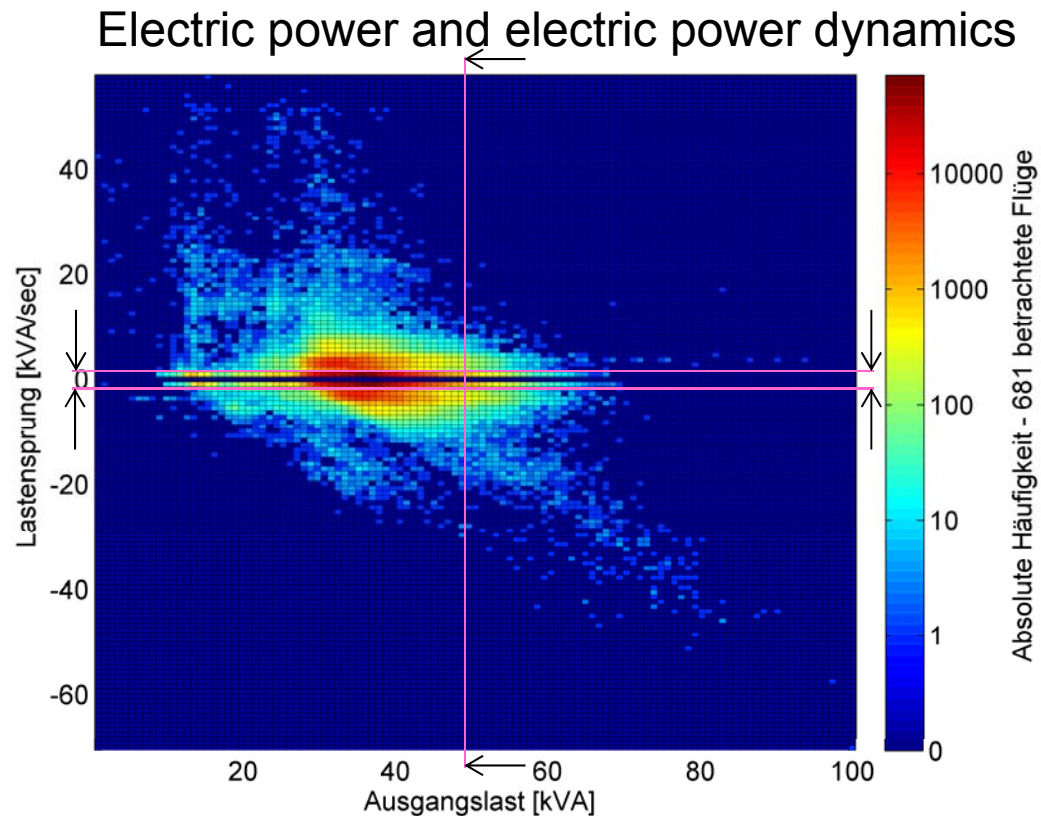


- Power slopes up to $\pm 50 \text{ kW/s}$
- Minor absolute power case $> 50 \text{ kW}$

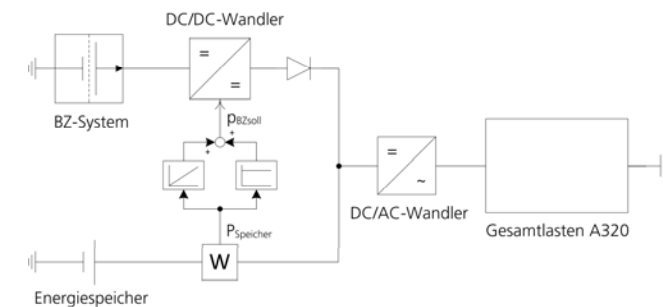
→ *Hybrid System*



Customized hybrid system for A320



Hybrid System – 50 KW FC



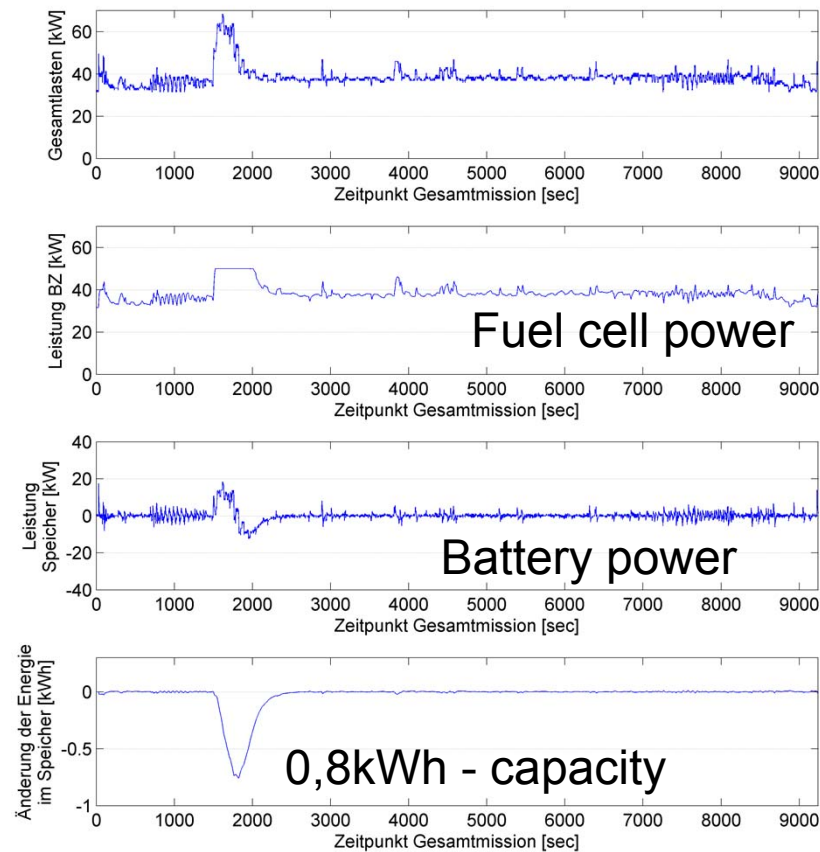
Hard boundaries FC dynamics
 → **1kW/s** power slope

Expected power from fuel cell system?
Power and capacity of used battery ?



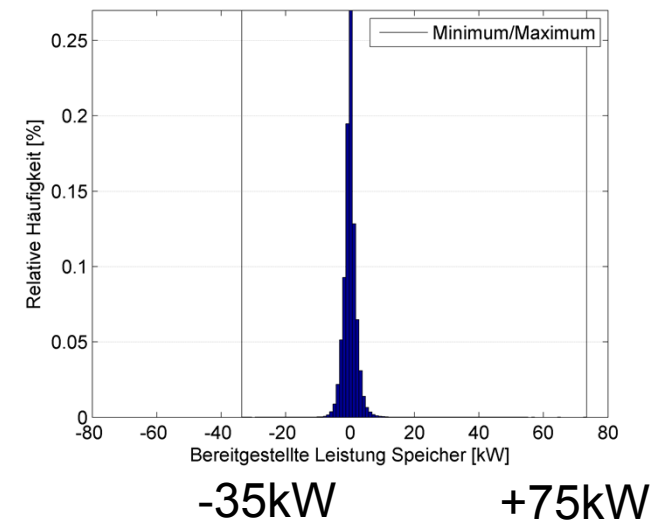
FC Hybrid system impact on battery power

A/C Power, fuel cell and battery power profile



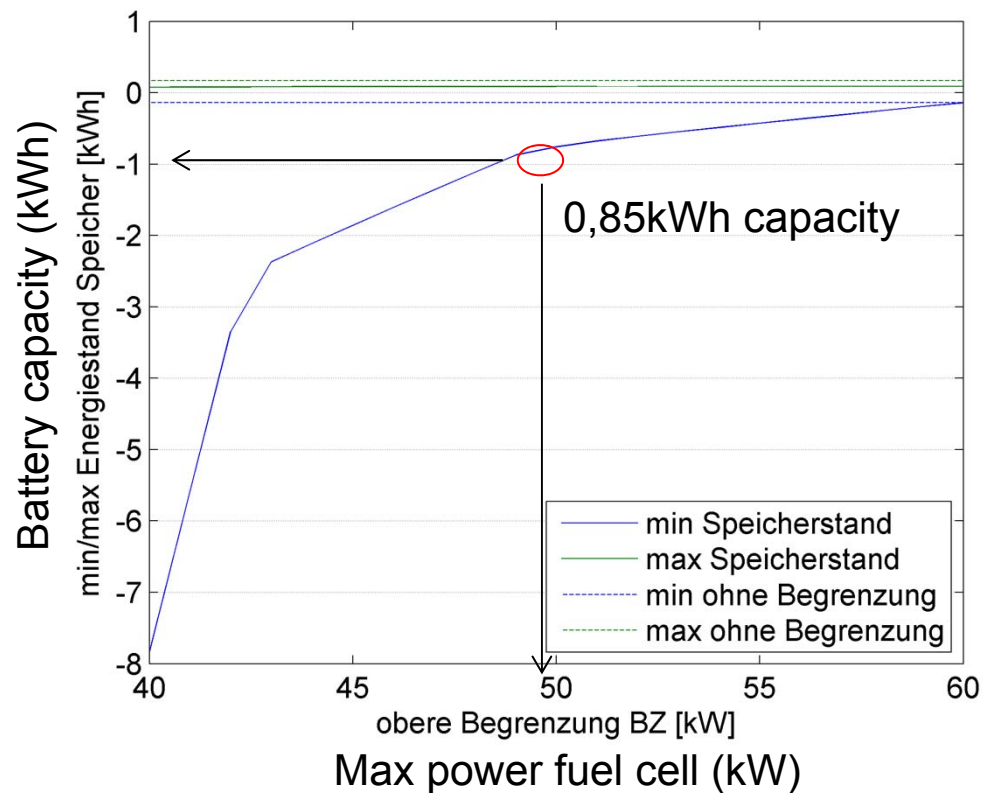
*FC Hybrid System - 50 KW
- 1kW/s*

Battery power: + 75kW ; - 35kW



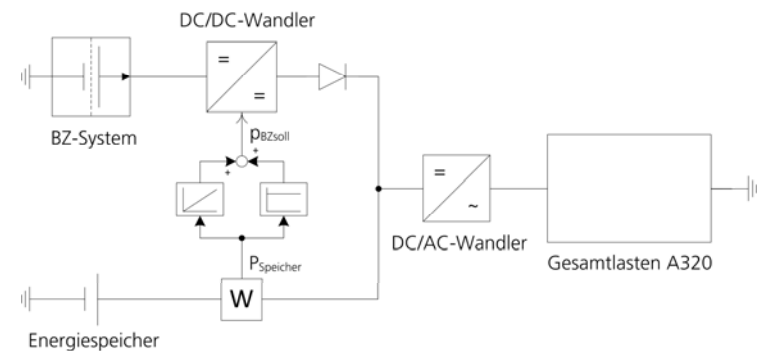
FC Hybrid System impact on battery capacity

Battery capacity as a function of max. FC system power

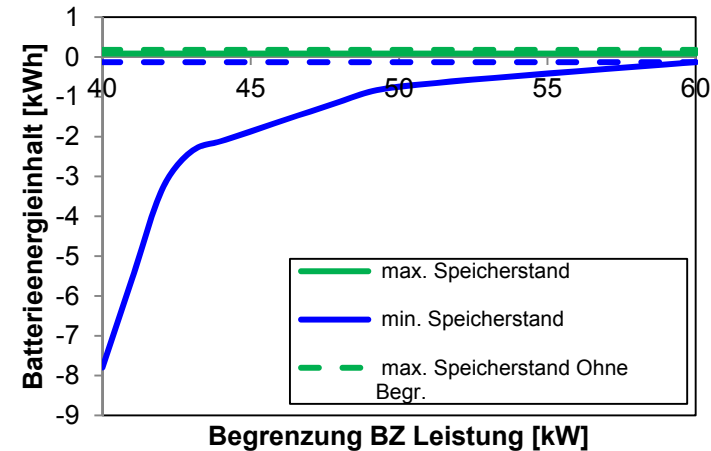
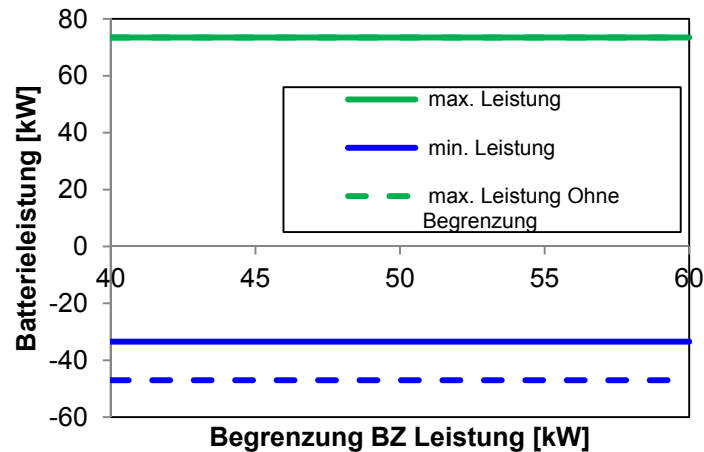


*FC Hybrid System - 50 KW
- 1kW/s*

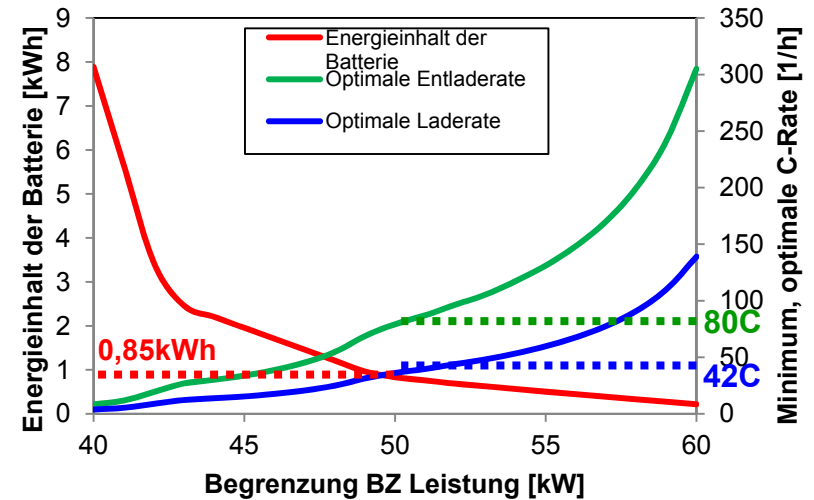
*Battery power: + 75kW ; - 35kW
Battery capacity: 0,85kWh (7kg)*



Abschätzung der idealerweise verfügbaren C-Rate



1. $E_{batt} \approx \overline{U_E} \cdot Q_{batt}, E_{Pack} = n_p \cdot n_s \cdot E_{batt}$
2. $P_{batt} = U(I, SOC) \cdot I(SOC), P_{Pack} = n_p \cdot n_s \cdot P_{batt}$
3. $\frac{P_{Pack}}{E_{Pack}} = \frac{P_{batt}}{E_{batt}} \approx \frac{U(I, SOC)}{\overline{U_E}} \frac{I}{Q_{batt}} = \frac{U(I, SOC)}{\overline{U_E}} \cdot I_{C-rate}$
4. $I_{C,opt} > \left. \frac{\overline{U_E}}{U(I, SOC)} \right|_{min, P_{Pack}=P_{Pack,max}} \cdot \frac{P_{Pack,max}}{E_{Pack}}$



Thank you for your attention!



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